

Rotating-Voltage-Vector Control for Wind Energy Plants providing Possibility for Ancillary Services Nastaran Fazli, Sidney Gierschner, Magdalena Gierschner, Lijun Cai, Hans-Günter Eckel

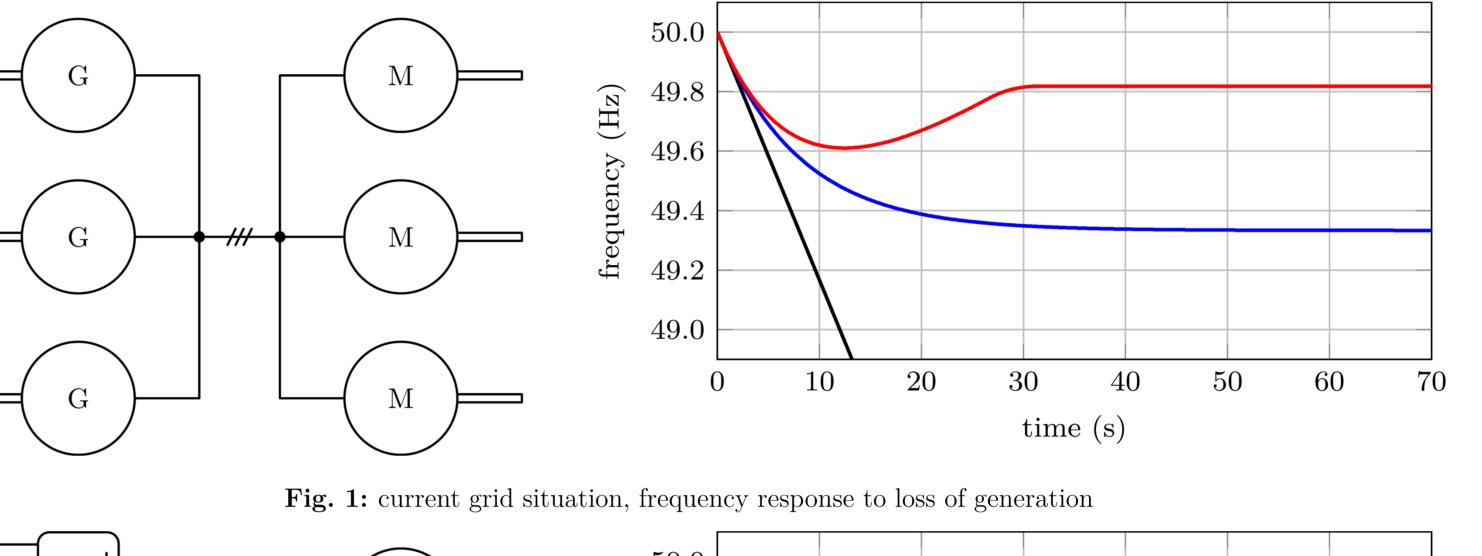
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Introduction

- conventional power plants supply instantaneous reserve using energy stored in rotating masses of the generators
- in case of a generation loss the drop of grid frequency is slowed down (Fig. 1, black line)
- grid self regulation effect (Fig. 1, blue line) and ancillary services supplied by power plants (Fig. 1, red line) will bring the grid frequency to a steady state
- just replacing conventional power plants by converter-based renewables will decrease the inertia in the grid
- renewables have to make contribution by participating in ancillary services
- providing virtual inertia to support frequency control
- grid-forming control schemes for grid-side converters to enable island grid operation and black start capability



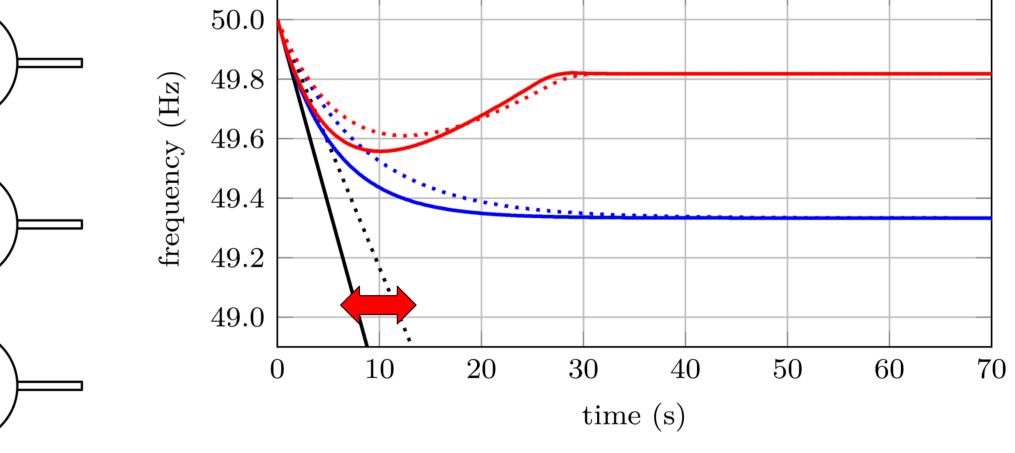
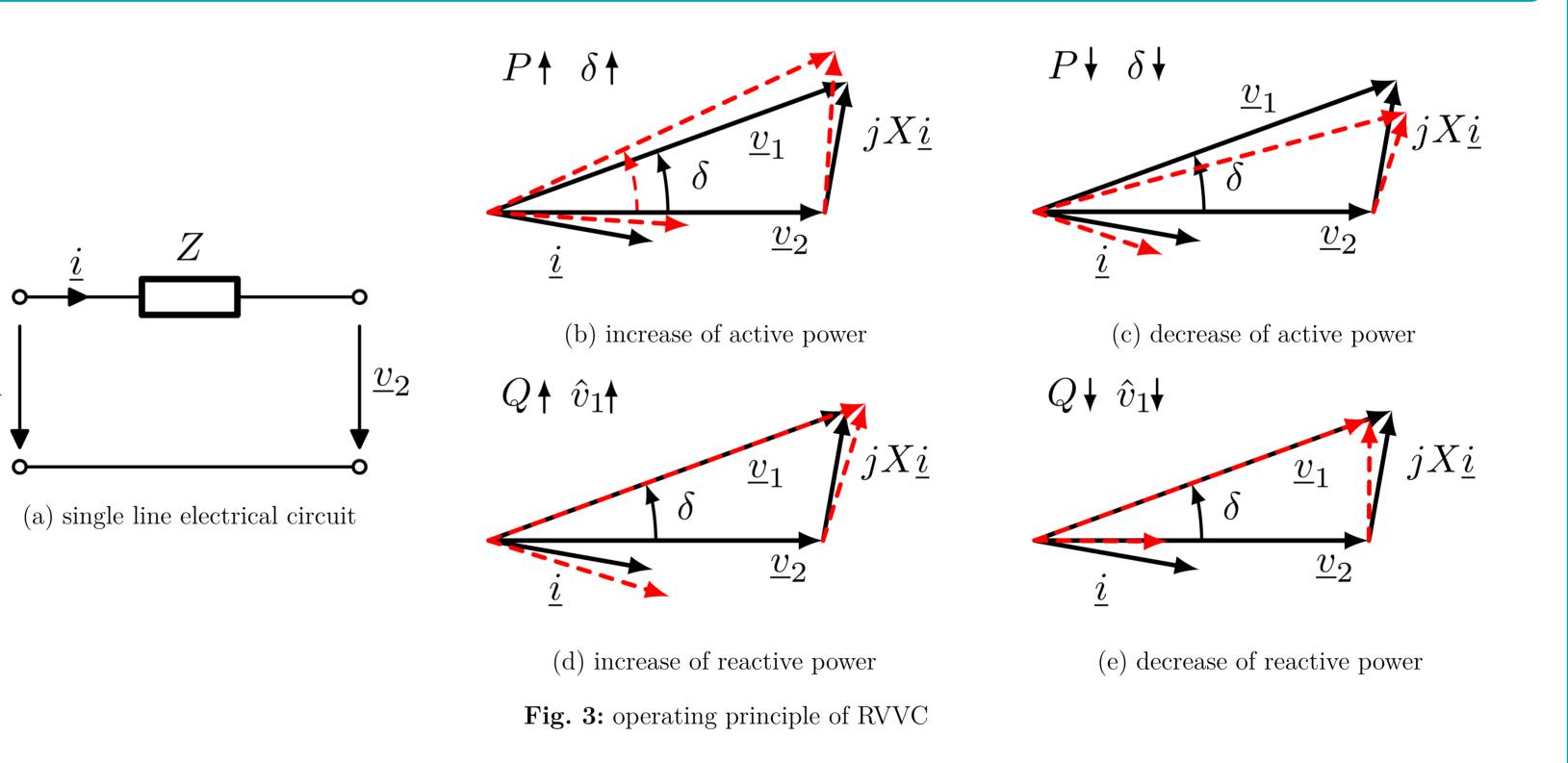


Fig. 2: change of grid situation, loss of inertia due to replacing power plants by converters

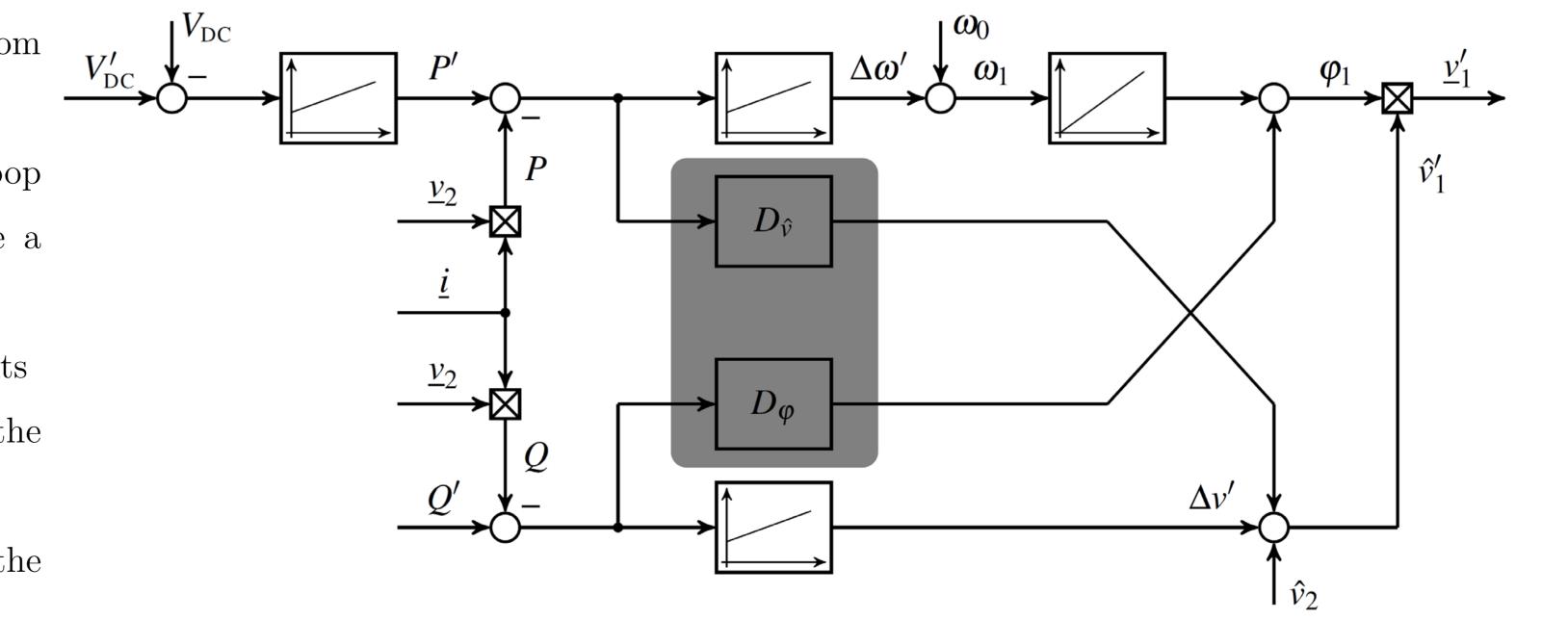
Operating Principle of Rotating-Voltage-Vector Control

- operation of a converter on the grid can be described by single line electrical circuit (Fig. 3a)
- converter \underline{v}_1 and grid \underline{v}_2 are connected via impedance Z
- active power P is primarily dependent on angle $\boldsymbol{\delta}$
- reactive power Q is primarily dependent on voltage \underline{v}_1 difference $\hat{v}_1-\hat{v}_2$
- power flow between grid and converter can be controlled by adjusting fundamental phase φ_1 and amplitude \hat{v}_1 of the converter voltage relative to the grid voltage



Control Structure of Rotating-Voltage-Vector Control

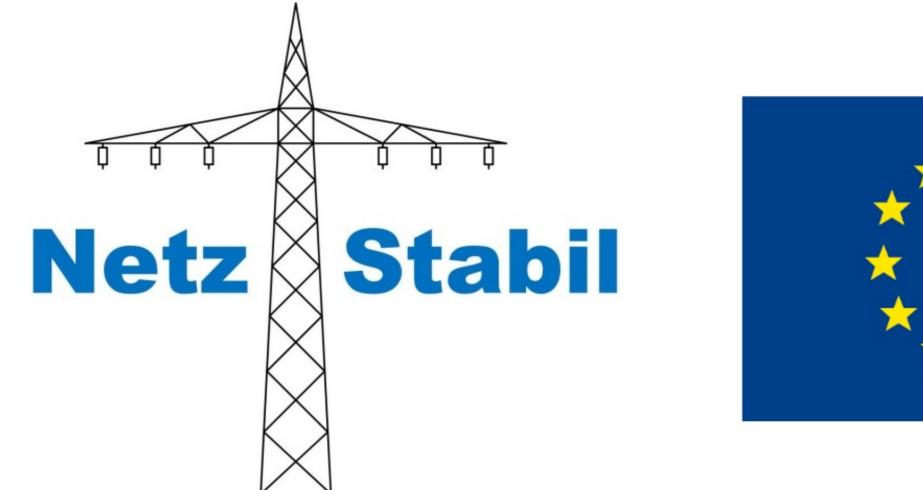
- instantaneous active and reactive power are calculated from measured grid voltage \underline{v}_2 and grid current \underline{i}
- reference value P' is specified by superordinate control loop



- of the DC-link voltage, which is intended to guarantee a constant DC-link voltage $V_{\rm DC}$
- reference value Q' is set according to external requirements
- a decoupling network $(D_{\hat{v}} \text{ and } D_{\varphi})$ is used to cancel the cross-coupling between P and \hat{v}_1 as well as Q and φ_1
- initial value of the angular frequency is set according to the desired grid frequency, usually 50Hz

Fig. 4: control structure of RVVC

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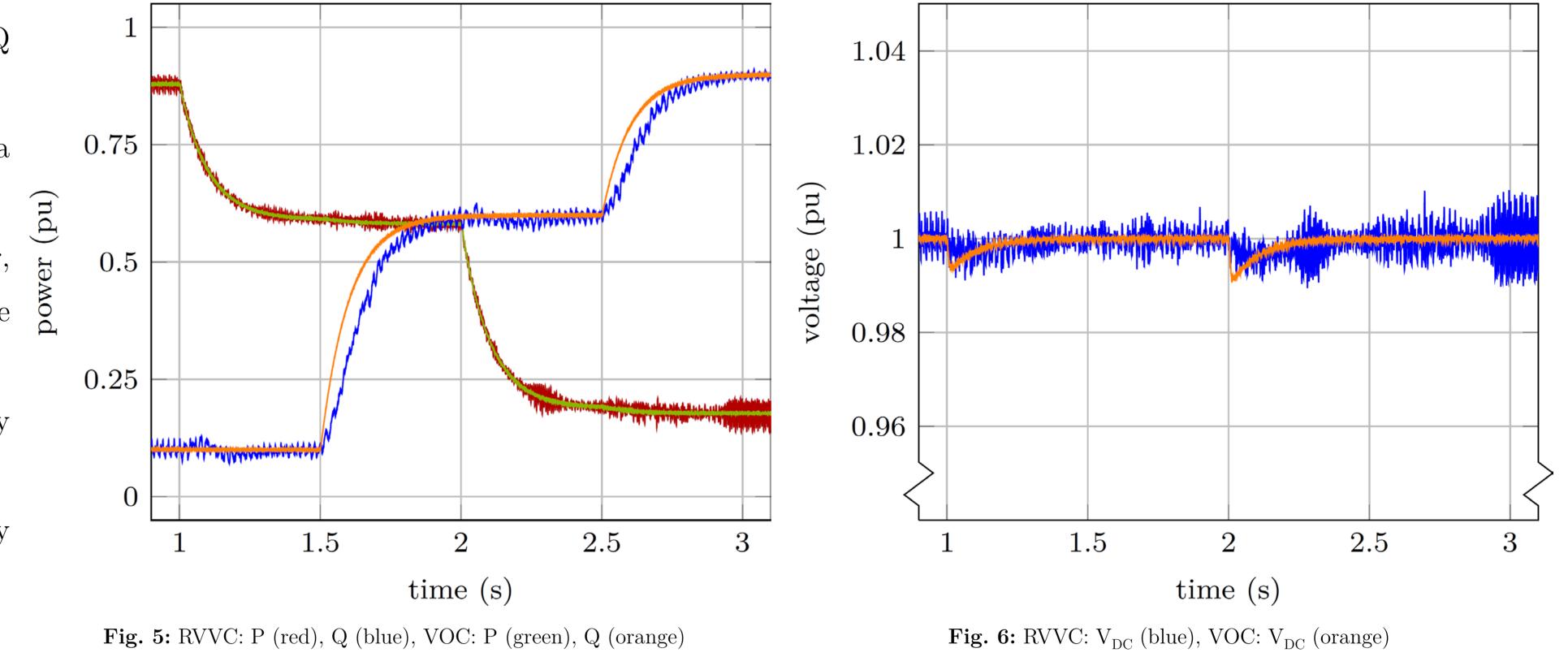


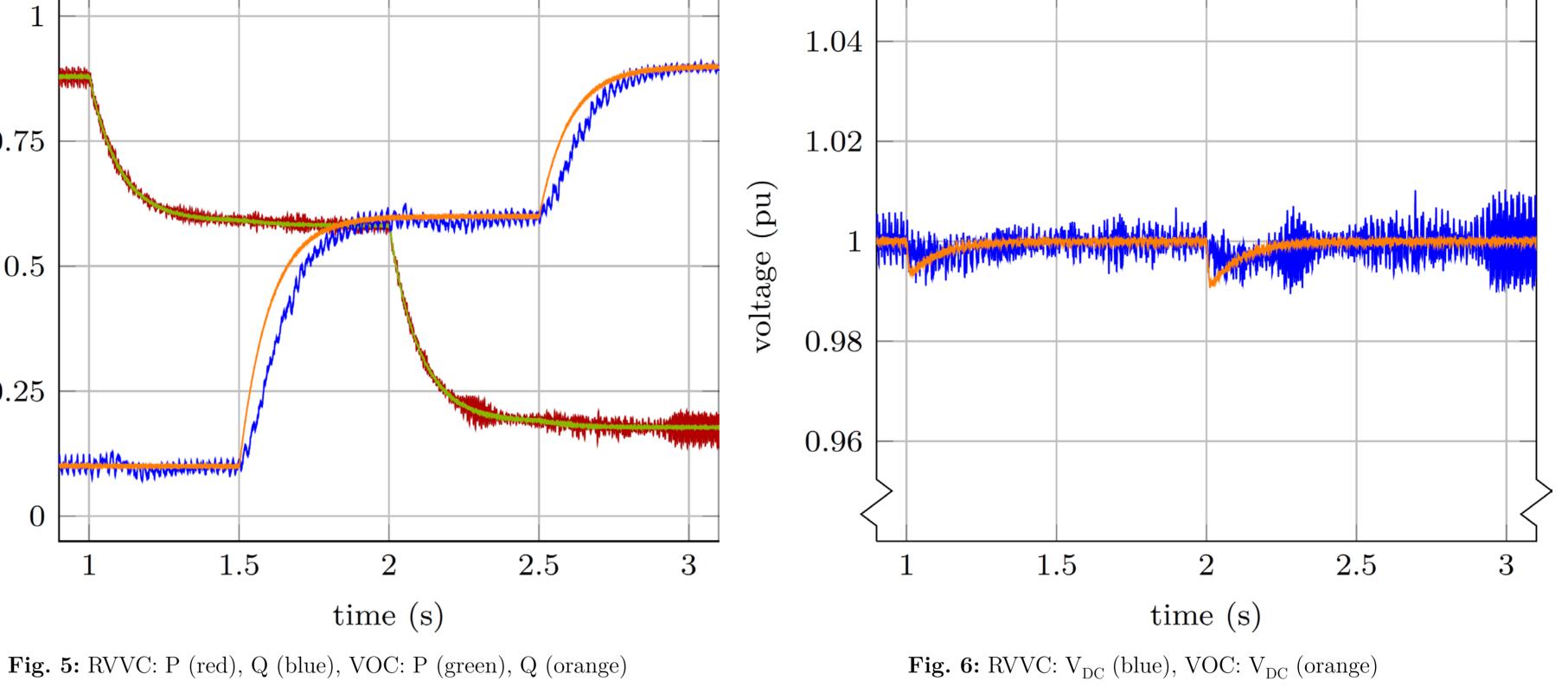
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Response to Changes in Active and Reactive Power

- VOC can track the changes of P and Q without problems
- active power control of RVVC shows a comparable behaviour power control is slower, • reactive

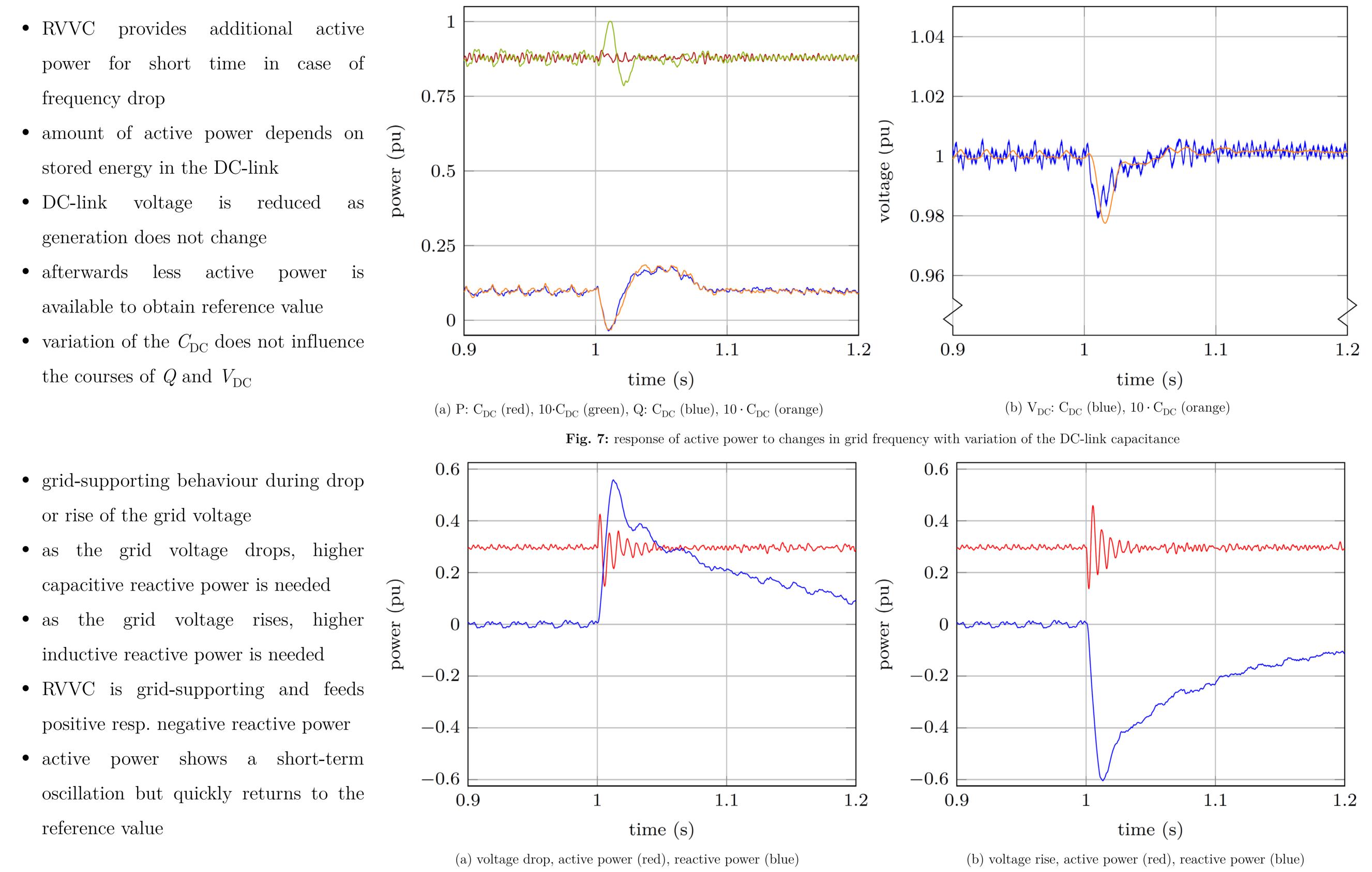




- controller design may be inadequate § and needs to be improved
- high proportion of low-frequency harmonics in active and reactive power
- drops of $V_{\rm DC}$ are compensated quickly for VOC and RVVC

Fig. 7: response to changes in active and reactive power

Response to Changes in Frequency and Voltage Amplitude of the Grid



Conclusion

- RVVC offers inherent short-term possibility of grid-supporting behaviour due to its internal structure
- RVVC is particularly suitable for decentralised regenerative feeders since it does not require grid synchronisation
- RVVC also enables island grid operation
- comparable results achieved with regard to state-of-the-art control schemes

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Fig. 7: response of reactive power to changes in amplitude of the grid voltage by 5%